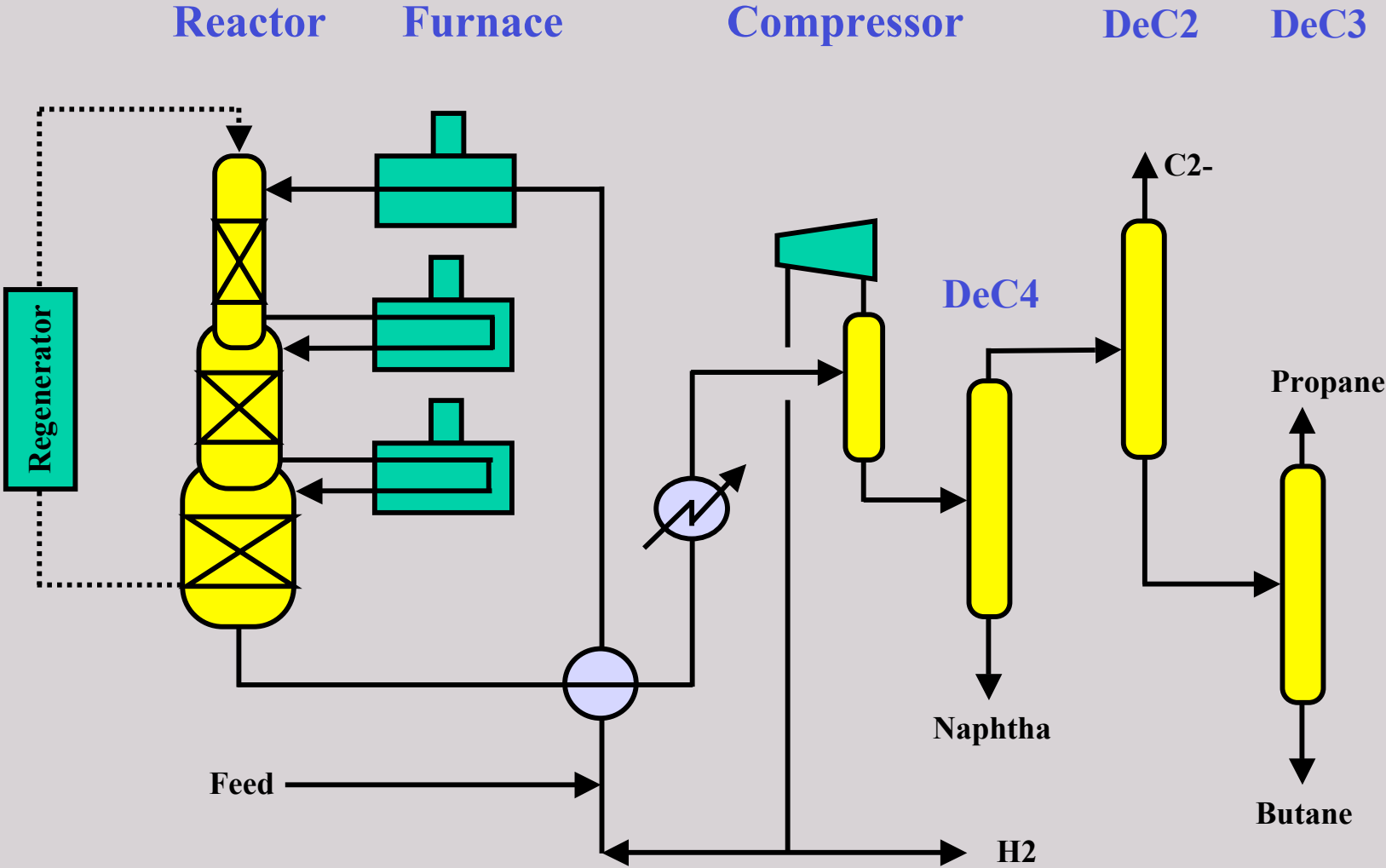


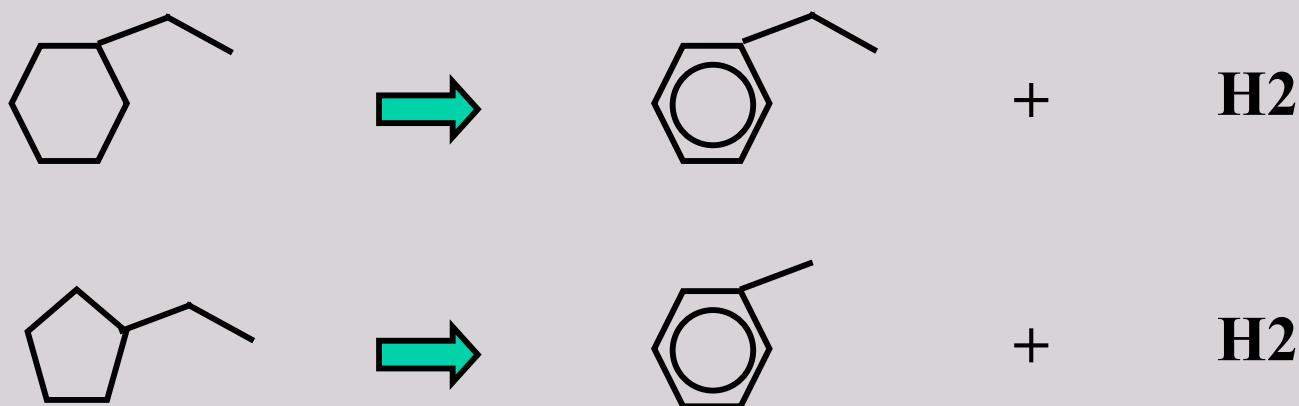
Petronas
Reformer paper
October 2007

H.K. Lim
Y. Zak Friedman
S.Y. Nam

Simplified reformer configuration



Aromatization



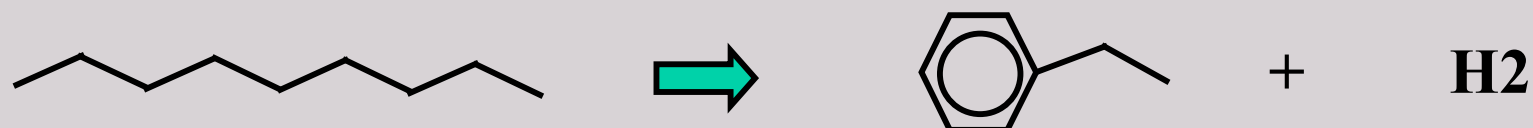
Main reaction, nearly 100% conversion

The naphtha product is very aromatic

➔ high octane

The reformer is a large producer of hydrogen

Dehydrocyclization



Difficult reaction, promoted by low pressure

NC6 reaction not very effective in semi-regenerative units, **~20% conversion**

CCR units (**low P**) **~50% conversion**

NC7 converts better, **40 - 80+% conversion**

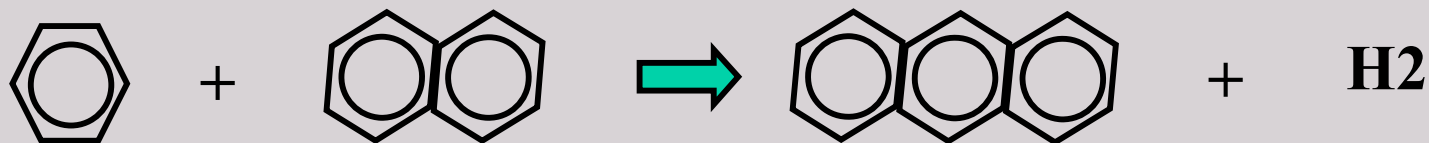
NC8 better yet, **70 - 95+% conversion**

Cracking side reaction



**Un-dehydrocyclized, low octane components,
are cracked**

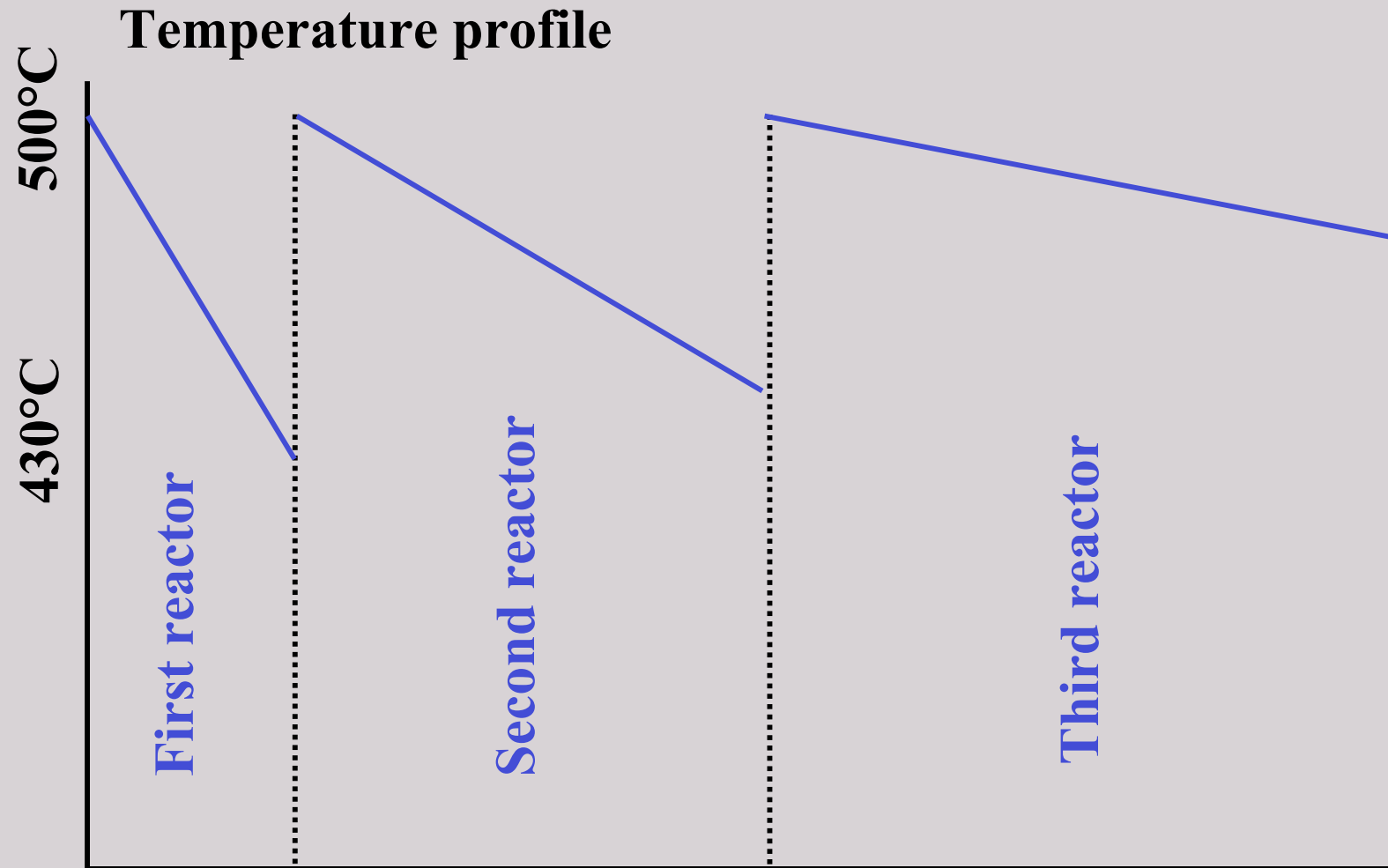
Aromatics condensation → Coke



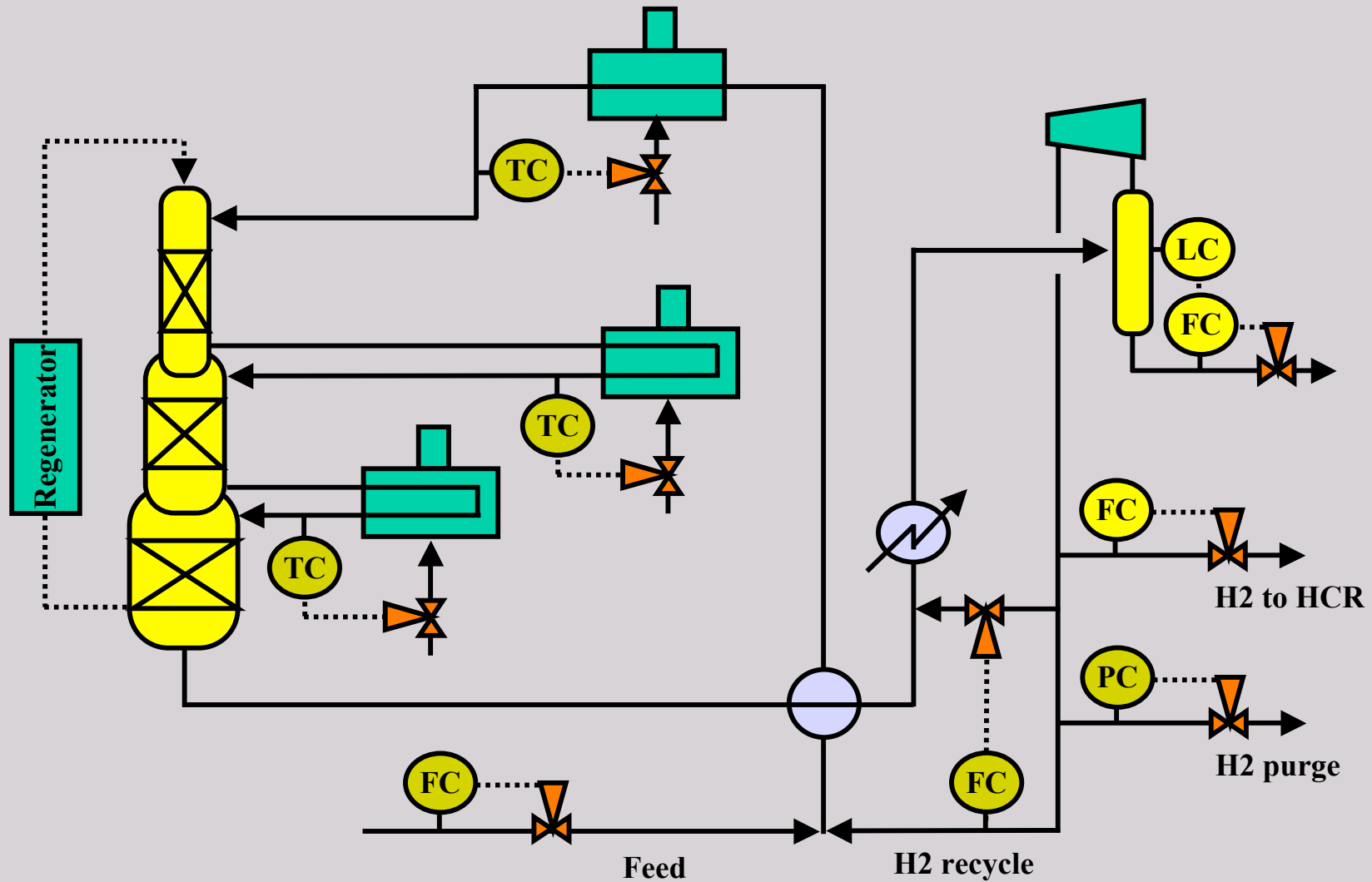
Coke gradually accumulates on the catalyst surface

Working with high ratio H₂ circulation to tilt the balance against coking

The reaction is endothermic



Main reactor controls



Reactor control

- **Control octane by changing WAIT**
 - (weighted average reactor inlet temperature)
 - Keep all inlets the same, except as needed to alleviate constraints
- **Control catalyst coking rate by manipulating hydrogen recycle ratio**
 - Keep the coking rate within the regenerator capacity
- **Regenerator reliability problem**
 - Frequent regenerator trips may dictate temporary throughput cuts

Manipulated variables

- **Reformer feed flow**
 - Maximize feed subject to reactor and NHT throughput constraints.
- **Reactor inlet temperatures**
 - Handles for controlling reactor severity
- **Recycle compressor suction valve**
 - Handle for controlling the hydrogen recycle ratio

Control variables – 1

- **Octane number calculation**
 - Octane inference is the main CV for controlling the reformat octane
- **Coke on catalyst laydown calculation**
 - Coke laydown inference may become an active constraint upon regenerator trip
- **Reactor inlet H₂/HC mole ratio**
 - Normally the H₂/HC ratio is set at 1.5, though it should be increase if there is a coke laydown problem

Control variables – 2

- **Throughput hydraulic constraints**
- **Recycle compressor constraints**
- **Reactor temperature profile CVs**
 - **Profile is to be respected subject to furnace constraints**
- **Furnace constrain CVs**
- **Certain NHT constraints**
 - **In rare situations the upstream naphtha hydrotreater may impose throughput limits on the reformer**

Control variables – 3

- **Hydrogen purge**
 - Half way through the project economic drives changed. The reformer is now operated solely for the purpose of supplying hydrogen
 - We added a hydrogen purge constraint to keep the purge low

This control relies on knowledge of octane and rate of coking

- **Octane measurement (or in our case inference) is a must**
 - **Keep catalyst coking rate within regenerator capacity**
 - **Steady octane operation improves yield**
- **Coking rate inference is good to have**
 - **Otherwise we must operate at a conservative hydrogen ratio**
 - **Affects unit efficiency and capacity**

What affects octane?

- **Feed boiling point**
 - Conversion increases with molecule size
- **PNA (paraffin – naphthene – aromatic)**
 - Aromatics ride through, they already have high octane
 - Naphthenes convert at 100% to high octane aromatics, but that conversion requires high reactor temperature
- **H2 recycle**
 - Partial pressure effect is minor

What affects coke make?

- **WAIT**
 - Coke make increases with reactor temperature, especially in the last reactor
- **H₂ recycle**
 - Partial pressure effect is major

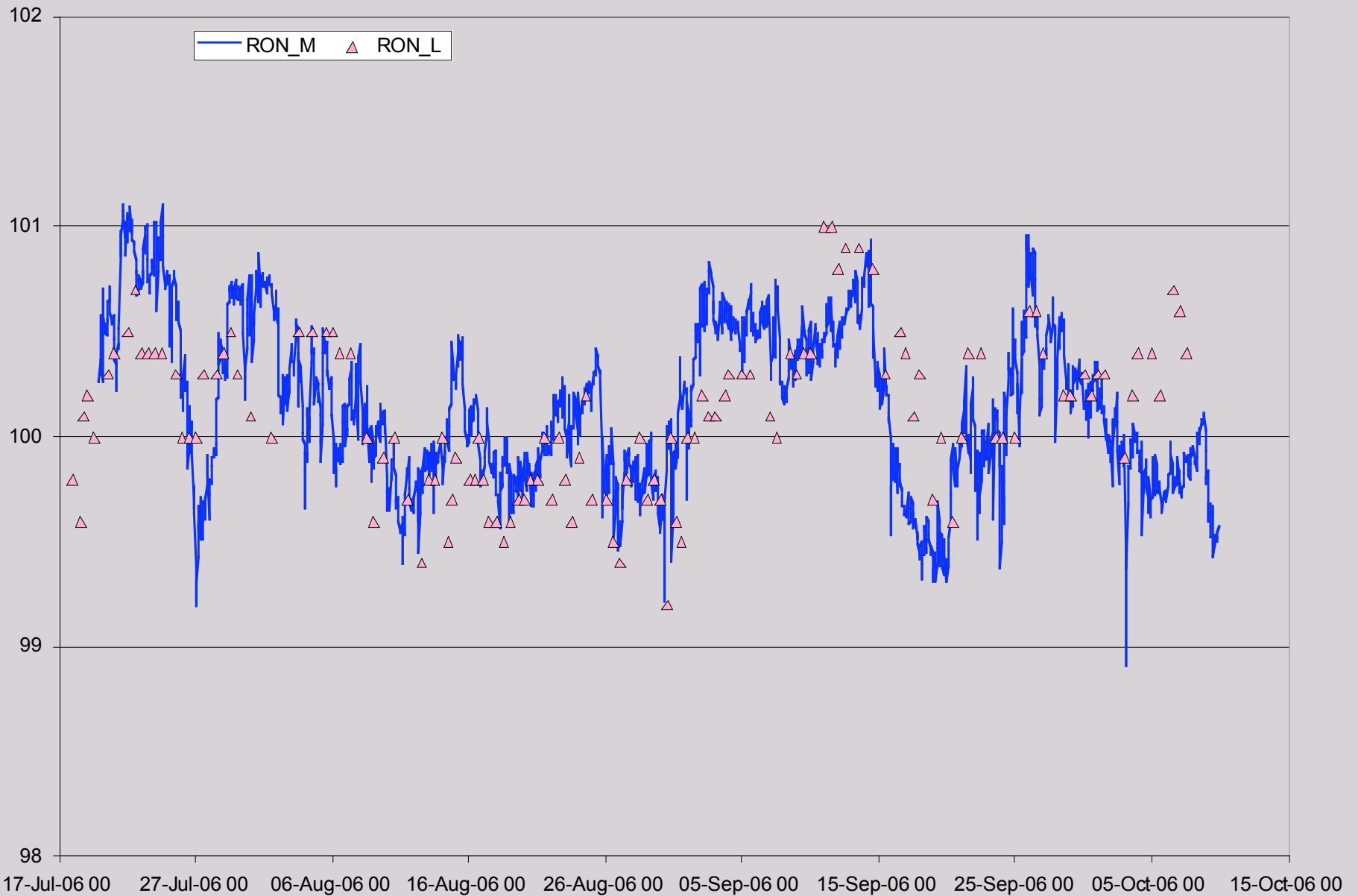
Inference of feed boiling point

- **Ideally feed boiling point should be inferred on the upstream crude unit**
 - **Not possible at Melaka because there are several feed sources**
 - **Inference is based on debutanizer bottom conditions, corrected for C4 and C5 separation**

Inference of feed PNA

- **Ideally feed PNA is inferred from**
 - Feed boiling range
 - Reactor conditions
 - Feed density
- **But the feed density analyzer is not installed yet, and the model assumes a constant PNA distribution**
- **Quality of octane inference is acceptable but not great**

Octane trend at Melaka



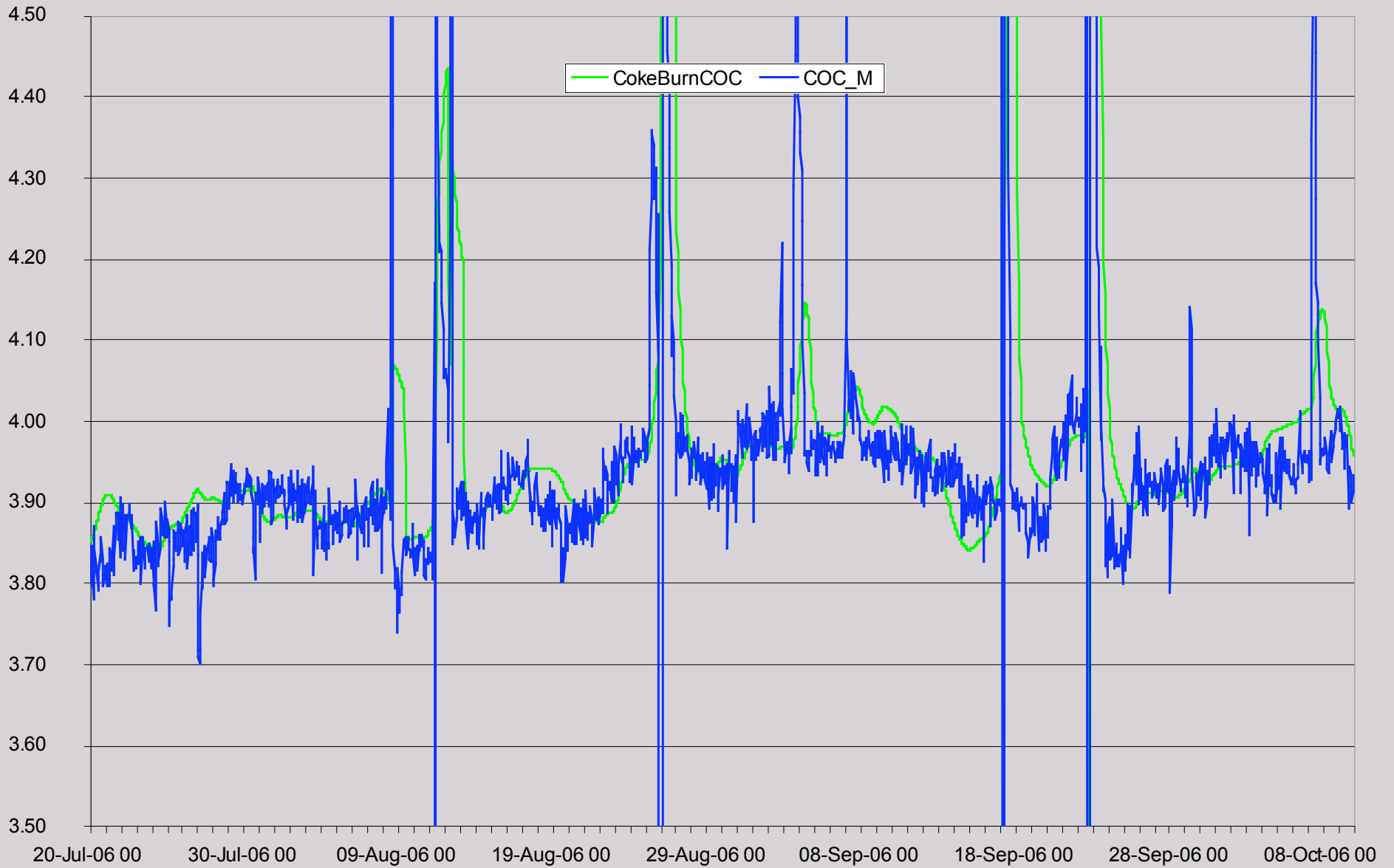
Octane trend at another location, incorporating density measurement



Coke deposit trend [Kg/Hr]



% coke on catalyst



How this application makes money?

- **At “normal” economic situation**
 - **Maximize feed at constant octane, considering reactor and regenerator constraints**
- **At current depressed economics**
 - **Minimize feed at constant octane to provide the needed H₂ supply while keeping H₂ purge at minimum**
- **A feed reduction of 5% was observed**

Conclusions

- Reforming is a sensitive high temperature catalytic process with many constraints
- APC of the reformer reactor requires reasonable inferences of
 - Reformate octane number
 - Catalyst coke deposit rate
- APC engineers must adjust applications for the economics of the day